



Heating Applications of Bio-Pellet Made from Ecological-Hazard Plant in Small and Medium Enterprises to Enhance Utilization of Renewable Energy in the APEC Region

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Steam based biomass gasification processes for syngas and hydrogen production

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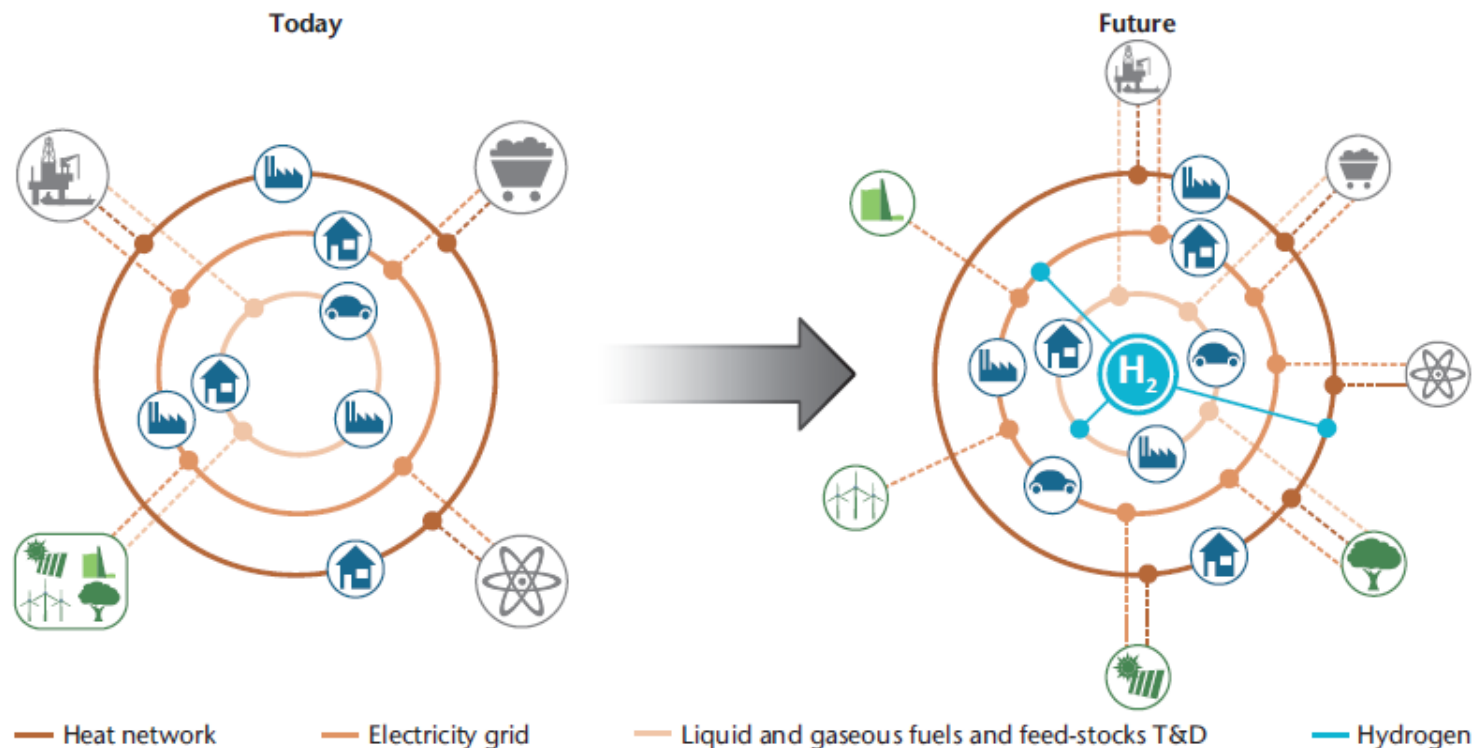
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✓ Potential of Hydrogen



➤ FCEV fleet (Targets) announced by hydrogen initiatives (2020)

Europe:~350 000, Japan:100,000, Korea:50,000, United States: ~20,000

Source: Technology Roadmap Hydrogen and Fuel Cells

OECD/IEA, 2015 International Energy Agency



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✓ Background

INPUT (Biomass)

Woody waste
Thinning
Sawmill waste
Cow dung
Livestock waste
Sewage sludge
etc.



OUTPUT (Product)

Hydrogen
or
Power & Heat



BLUE Tower II – Third pilot plant

(Shibukawa Technology Development Center of JBEC*)

*Japan Blue Energy Co. Ltd.

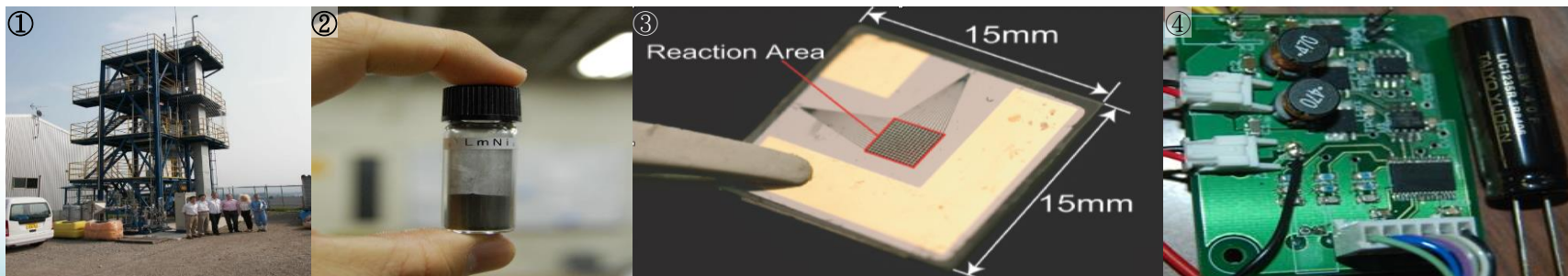
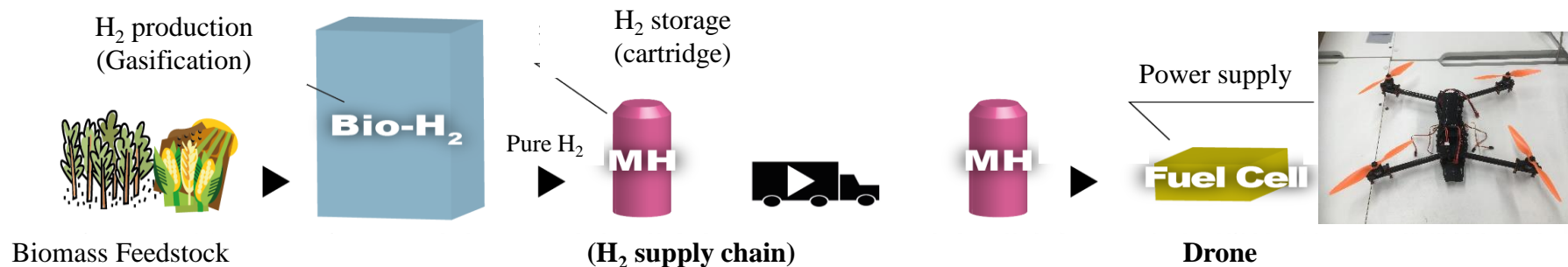
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✓ Our Strategy -R&D of Fuel Cell Drone by Bio-H₂ fuel supply-

- ① Combination of Bio-H₂ production technology and a cell phone
- ② Expansion of Bio-H₂ application.

Prof. K. Dowaki (Project leader)	: Gasification technology, Gas Cleaning Technology · LCA
Prof. T. Gunji	: Removal technology of contaminants in Bio-syngas
Prof. M. Hayase	: Small scale PEFC in consideration of CO and H ₂ S tolerance
Dr. N. Katayama	: H ₂ storage system (metal hydride) · power converter circuit



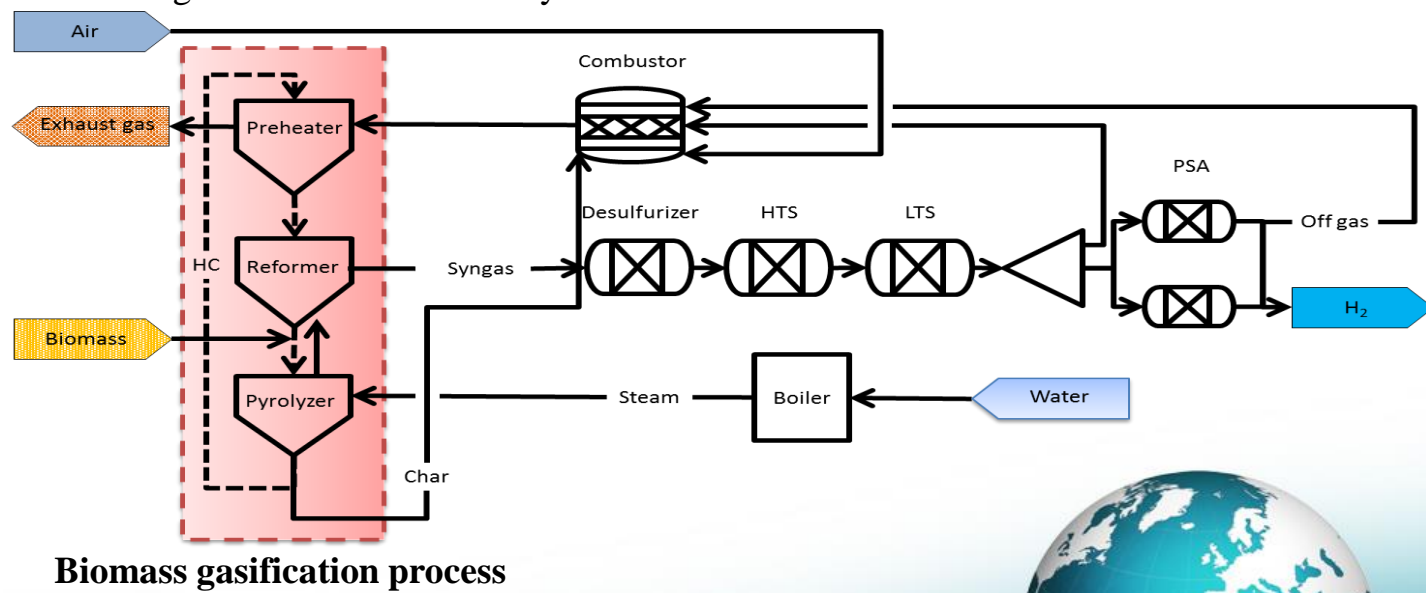
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✓ Gasification Technology

Basic contents

- The gasifier type is the biomass pyrolysis system in a reductive atmosphere.
- The system has 2 furnaces of pyrolysis+reforming zone and pre-heater.
- H_2 concentration in syngas would be comparatively high (>40 vol.%).
- The plant capacity would be the range of 5 to around 70 t/day.



Our tasks in this study

- Confirmation of syngas yields and concentrations due to experiments.
- Confirmation of adsorption performance due to experiments. (CO_2 adsorption / H_2 purification)
- Process design of H_2 production system and estimations of production rate and auxiliary power
- Removal of impurities in syngas.
- Calculation of Eco-footprint of Bio- H_2 on basis of LCA concept.



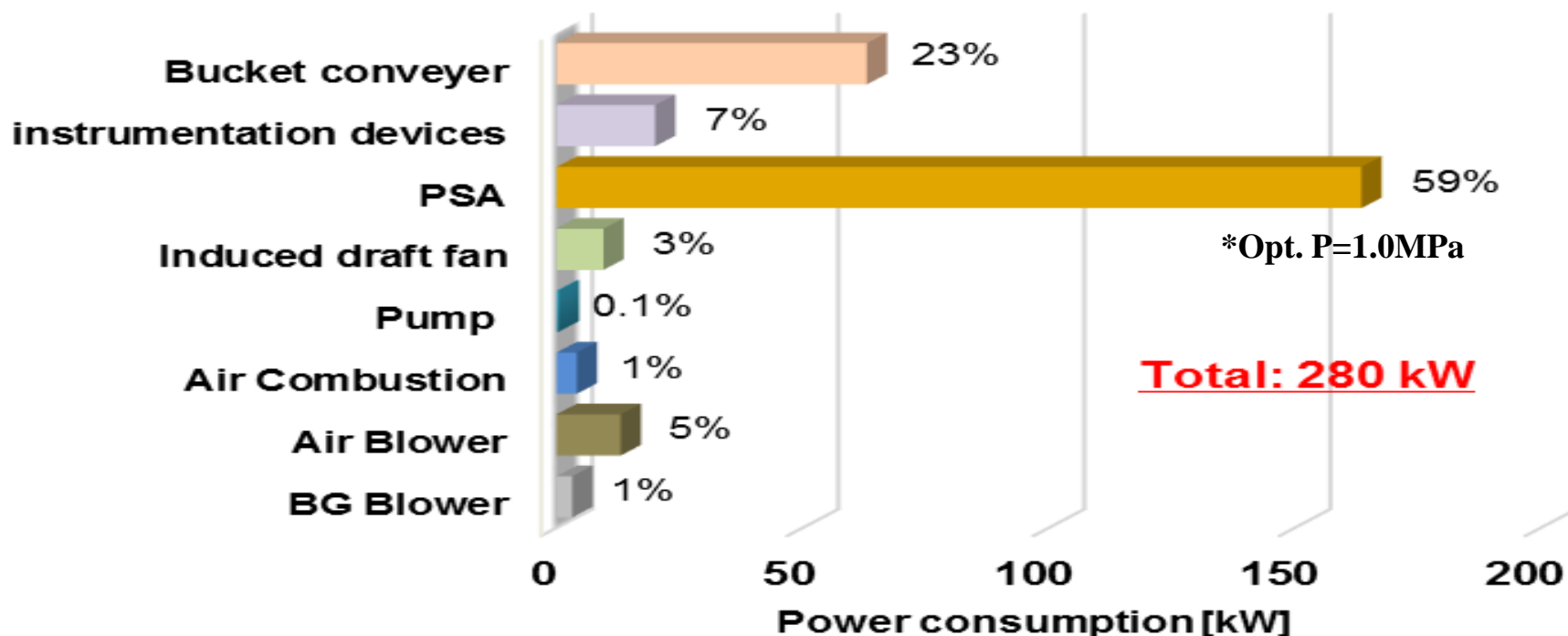
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✓ Reduction of auxiliary in Bio-H₂ plant

- In the previous LCA study on BT process design in use of the simulator of ASPEN-PLUS, we clarified that **the highest impact energy consumption is due to the auxiliary power of PSA.**

Reduction of energy consumption by our proposals will be achieved.





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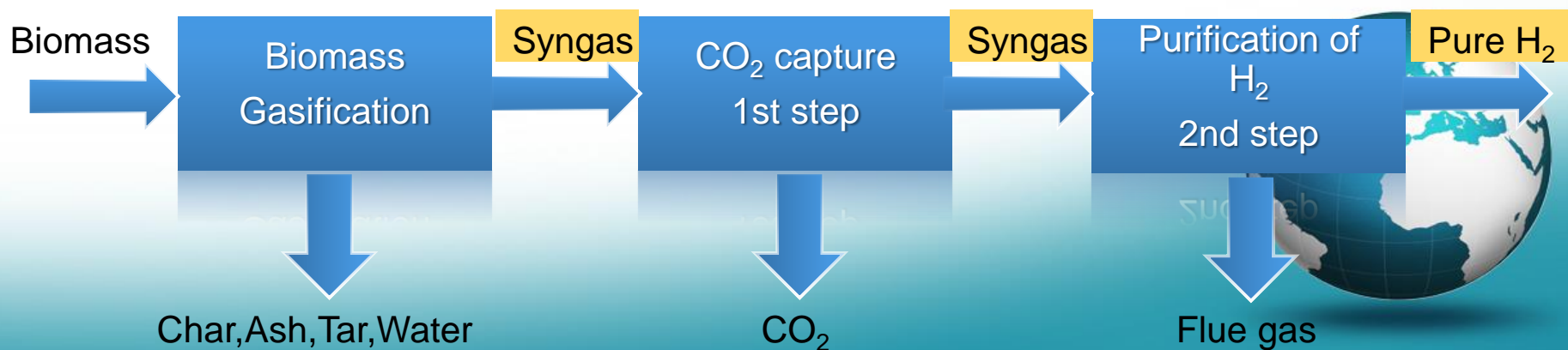
✓ Development of 2-step PSA

□ Performance test in use of “2-step PSA apparatus”

- ① Confirmation of gaseous yields and concentrations
- ② Preparation of bio-syngas
- ③ Execution of adsorption tests
 - Different species of absorbent (form and pore)
 - 2-step PSA controls (pressure and temperature)
 - Combination of absorbents



- a. Power saving due to low pressure/low temperature controls and a reduction of amount of a working gas fluid (ex. 0.8MPaG->0.5MPaG, CO₂ removal)
- b. Achievement of CO₂ adsorption and H₂ purification with higher efficiencies

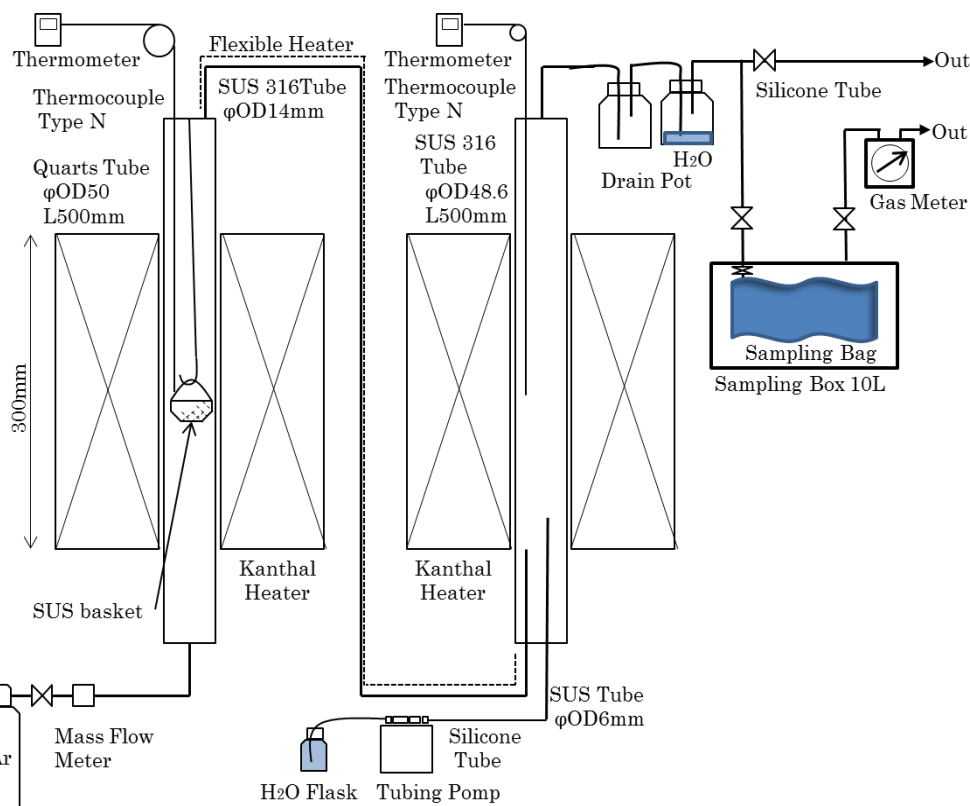


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✓ Fabrication of apparatus (Gasification Process)

- Confirmation of the performance
- Data acquisition for the static modeling (AspenPlus)



Proximate Analysis	Waste W		J. cedar (Reference)
Moisture	6.02	wt.%	37.70
Ash	0.35	wt.%	2.20
Volatiles	82.92	wt.%	83.50
Fixed carbon	10.71	wt.%	14.30

Ultimate analysis			
Carbon	50.9	wt.%	50.41
Hydrogen	7.3	wt.%	5.52
Nitrogen	0.13	wt.%	0.31
Oxygen	41.27	wt.%	43.76
Chlorine	0.01	wt.%	0.01
Sulfur	0.01	wt.%	0.02

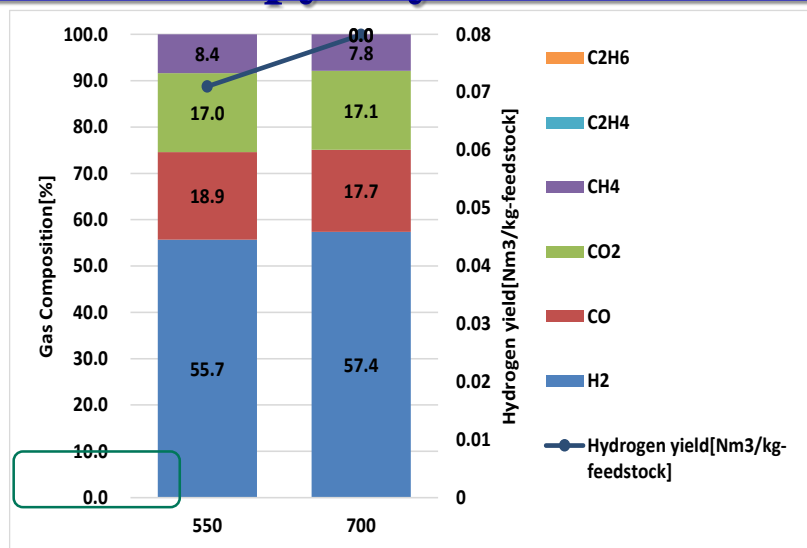
Measurement of gaseous yields

Note: This apparatus consists of pyrolysis zone and reforming zone.

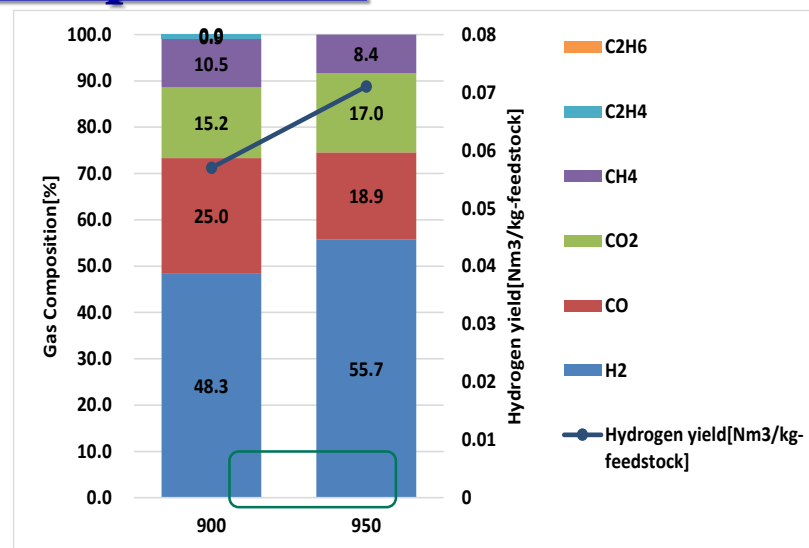
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✓ Effects of pyrolysis and reforming temperatures



Pyrolysis Temp. [deg.C](Reforming T=950)



Reforming Temp [deg.C] (Pyrolysis T=550)

Performance (summary)

Pyrolysis Temp. [deg.C]	550	550	700
Reforming Temp. [deg.C]	900	950	950
Syngas [L/g-feedstock]	1.02	1.10	1.19
Char [g/g-feedstock]	0.2	0.2	0.2
Tar [g/g-feedstock]	0.02	0.04	0.008
Cold gas efficiency [%]	71	68	73



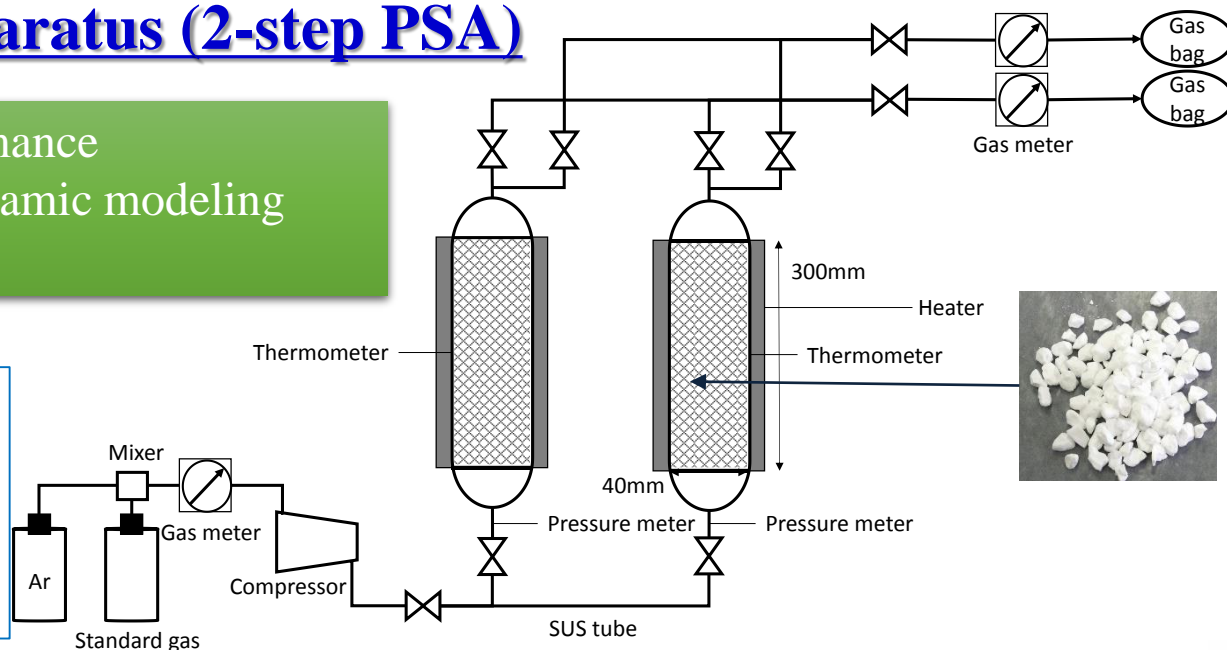
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✓ Fabrication of apparatus (2-step PSA)

- Confirmation of the performance
- Data acquisition for the dynamic modeling (gPROMS)

- Adsorbent volume : 200 ml
- Opt. Temp. : RT
- Opt. P : 0.4 MPaG
- Feed gas : H₂ 55%, CO 20%, CH₄ 8%, CO₂ 17%
- Opt. time : 5 min



Measurement of PSA performance

Adsorbents characteristic

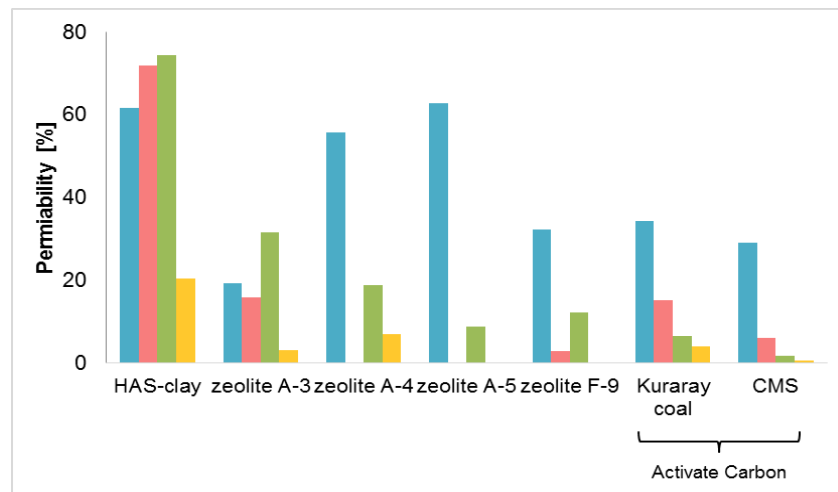
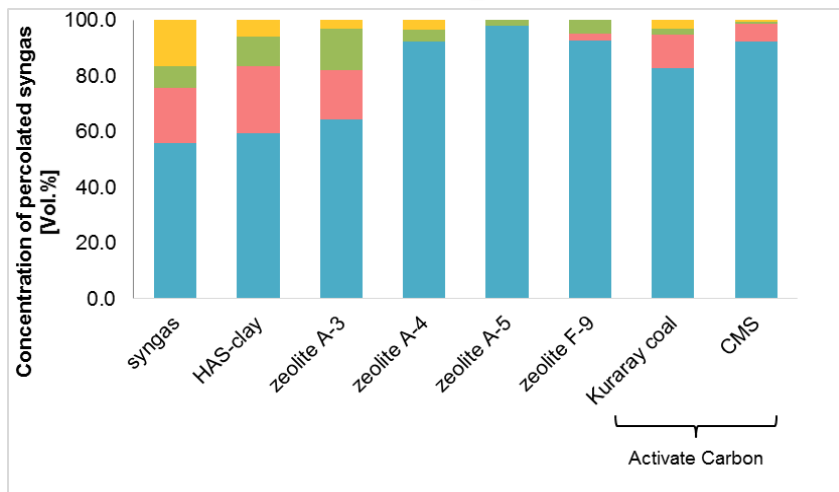
Specification	HAS-Clay	Zeolite A-3	Zeolite A-4	Zeolite A-5	Zeolite F-9	Activated carbon (Kuraray Coal)	Activated carbon (CMS)
Chemical composition	$\text{SiO}_2 \cdot \text{Al}_2\text{O}_3 \cdot \text{H}_2\text{O}$	$\text{MeO} \cdot \text{Al}_2\text{O}_3 \cdot m\text{SiO}_2 \cdot n\text{H}_2\text{O}$ (Me: Cation)				Carbon	Carbon
Particle size [mm]	>2.0	2.36-4.75	2.36-4.75	2.36-4.75	2.39-4.75	4-5.5	2.36-4.75
Pore diameter [nm]	<0.02	0.3	0.4	0.5	0.9	0.5-10	0.5



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✓ Result of adsorption test (1)



<HAS-clay>

- ✓ Only CO₂ permeability was worse in comparison to the other gas components.
- ✓ That of H₂ was relatively higher.

<Zeolite A-5>

- ✓ The gaseous components percolated in the absorbent were H₂ and CH₄.
- ✓ H₂ permeability was highest among the candidates.
- ✓ The concentration of H₂ which passed through Zeolite A-5 was 90% or more.



Our proposals

- At the 1st step, **HAS-clay** is employed in order to adsorb **CO₂** selectivity.
- At the 2nd step, **Zeolite A-5** is employed in order to purify **H₂**.



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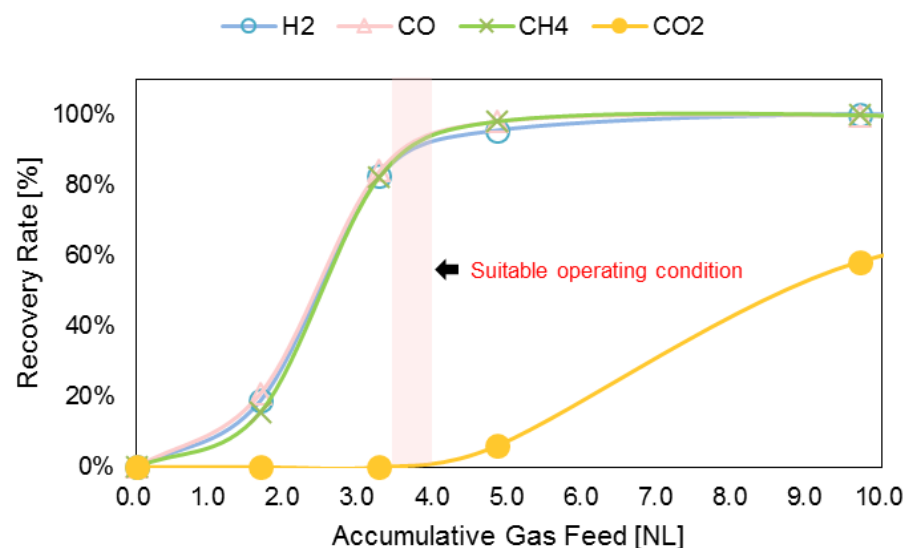
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✓ Result of adsorption test (2)

In order to make only CO₂ component separated from HAS-clay at 1st step, the breakthrough curve was measured.

<Condition>

- ✓ Gas flow rate
(Syngas(10%)+Ar(90%)) : 13.1 NL/min
- ✓ Operating pressure
: 0.4 MPaG
- ✓ Operating temperature
: Atmospheric (28 to 32 deg.C)
- ✓ Amount of HAS-clay
: 200 cc



- ↓
- H₂ and CO₂ are likely to be separated individually by the combination of HAS-clay at 1st step with Zeolite A-5 at 2nd step, and the gas flow control in consideration of CO₂ retention time.



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✓ LCA study on Bio-H₂ production

- Based on our experimental results, we designed the process of target system.
- We argued the optimal condition in consideration of LCA concept.

<Definition of Eco footprint>

H₂ fuel production efficiency[%]

$$\eta_{energy} = \frac{Q_{H_2}}{W_1 + W_2 + H_1(T_1) + H_2(T_2) + Q_{syn} - Q_{og}}$$

CO₂ emission of H₂ fuel [g-CO₂/MJ-H₂]

$$FCO_2 = \frac{C_1 + C_2 + C_{aux} - \alpha C_{fs}}{Q_{H_2}}$$

The coefficient of α can be set up by the test of CO₂ assimilation in use of model plant (e.g. Arabidopsis thaliana).

Q_{H_2} : LHV of H₂ [MJ/h]

Q_{syn} : LHV of syngas [MJ/h]

Q_{og} : LHV of off gas [MJ/h]

W_1 : first step of PSA [MJ/h]

W_2 : second step of PSA [MJ/h]

$H_1(T_1)$: sensible heat of first reactor [MJ/h]

$H_2(T_2)$: sensible heat of first reactor [MJ/h]

C_1 : CO₂ emission of first reactor [g-CO₂/h]

C_2 : CO₂ emission of second reactor [g-CO₂/h]

C_{aux} : CO₂ emission of auxiliary [g-CO₂/h]

C_{fs} : CO₂ emission due to carbon neutral [g-CO₂/h]

α : the percentage of adsorbed CO₂ gas [-]

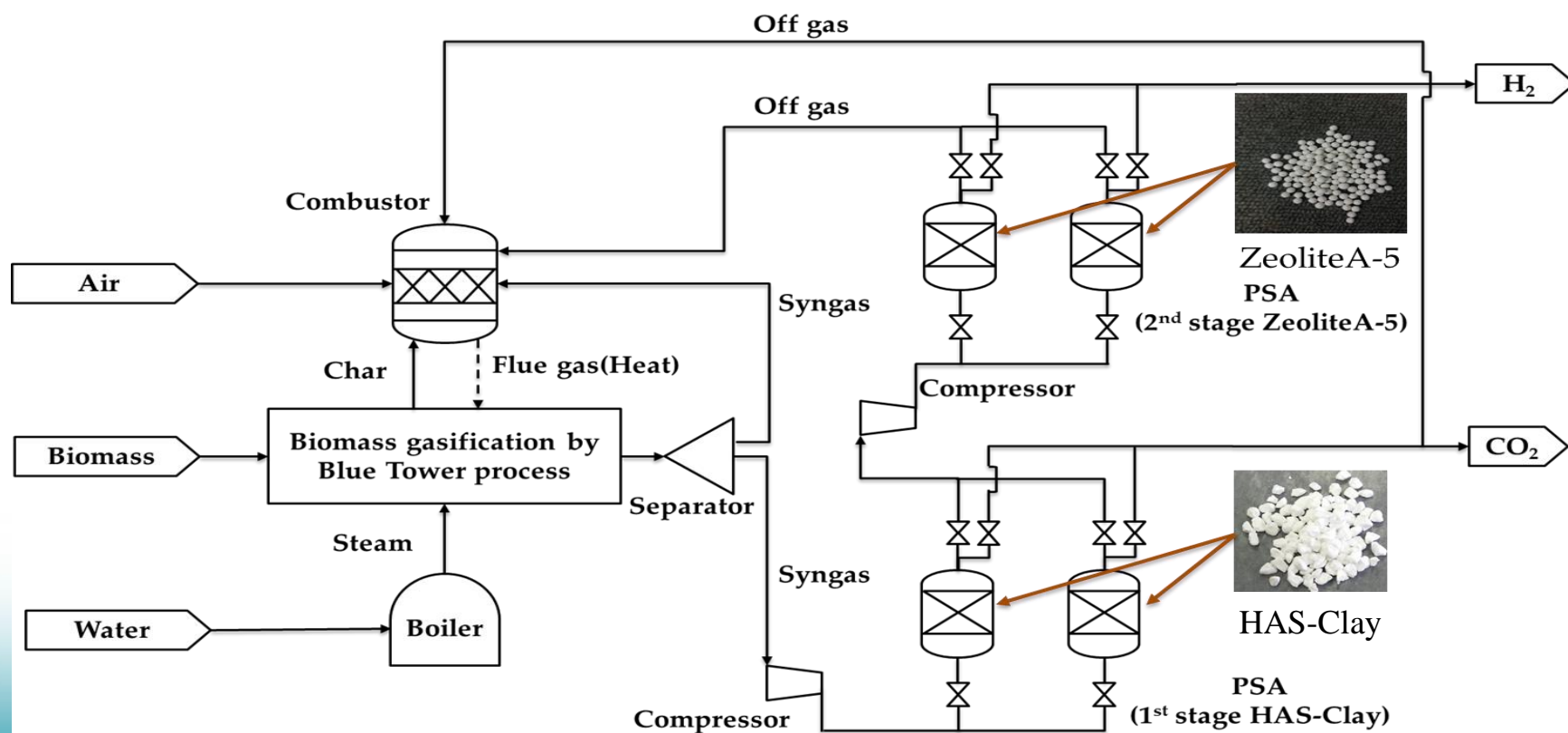
- In the case of the combination of HAS-clay with Zeolite A-5,
- ✓ η_{energy} : 82.8%, FCO_2 : -56.6 g-CO₂/MJ-H₂ (164kW→112kW, Reduction by 31%)
- In the conventional case⁽¹⁾,
- ✓ η_{energy} : 79.0%, FCO_2 : 57.4 g-CO₂/MJ-H₂

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✓ Dynamic Simulation of 2-step PSA

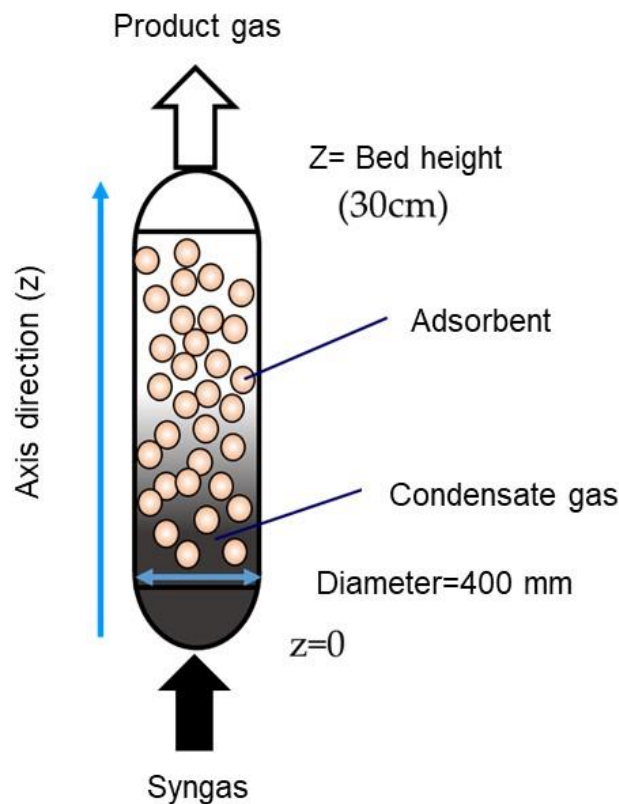
- 1st stage, CO₂ adsorption
- 2nd stage, H₂ purification



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✓ Modeling



Fig, Schematics model

● Mass balance

$$\underbrace{\varepsilon_{bed} \frac{\partial C_{g,i}}{\partial t}}_{\text{Non constant}} = \underbrace{\frac{\partial}{\partial z} (\varepsilon_{bed} D_{ax,i} \frac{\partial C_{g,i}}{\partial z})}_{\text{Diffusion}} - \underbrace{u \frac{\partial C_{g,i}}{\partial z}}_{\text{Convection}} - \underbrace{(1 - \varepsilon_{bed}) a_p k_f (C_{g,i} - C_{s,i})}_{\text{Adsorption}}$$

● Heat balance

Consideration of heat transfer between surface of inner vessel and gas flow.

$$\underbrace{(\varepsilon_{bed} C_g C_p g + \rho_{bed} C_p s) \frac{\partial T}{\partial t}}_{\text{Non constant}} = \underbrace{-\frac{\partial}{\partial z} (K_L \frac{\partial T}{\partial z})}_{\text{Diffusion}} + \underbrace{\varepsilon_{bed} C_g C_p g \frac{\partial T}{\partial z} u}_{\text{Convection}} + \underbrace{\rho_{bed} \sum_{j=1}^{Comp} \Delta H_j \frac{\partial q_j}{\partial t}}_{\text{Heat generation}} + \underbrace{\frac{2h_w}{R_{in}} (T - T_{wall})}_{\text{Surface - gas flow}}$$

● Pressure loss(Blake-Kozeny)

$$-\frac{\partial P}{\partial z} = 180 \frac{\mu(1 - \varepsilon_{bed})^2}{\varepsilon_{bed}^3} \frac{\mu u}{D_p^2}$$

● gPROMS (finite element method)



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✓ Simulation conditions

- PSA Cycle: Compression->Refinery->Decompression->Purge
- Number of cycles (in this simulation): 3

Note: Simulation parameters (physical properties) are used by the reference data ^{[1][2]}

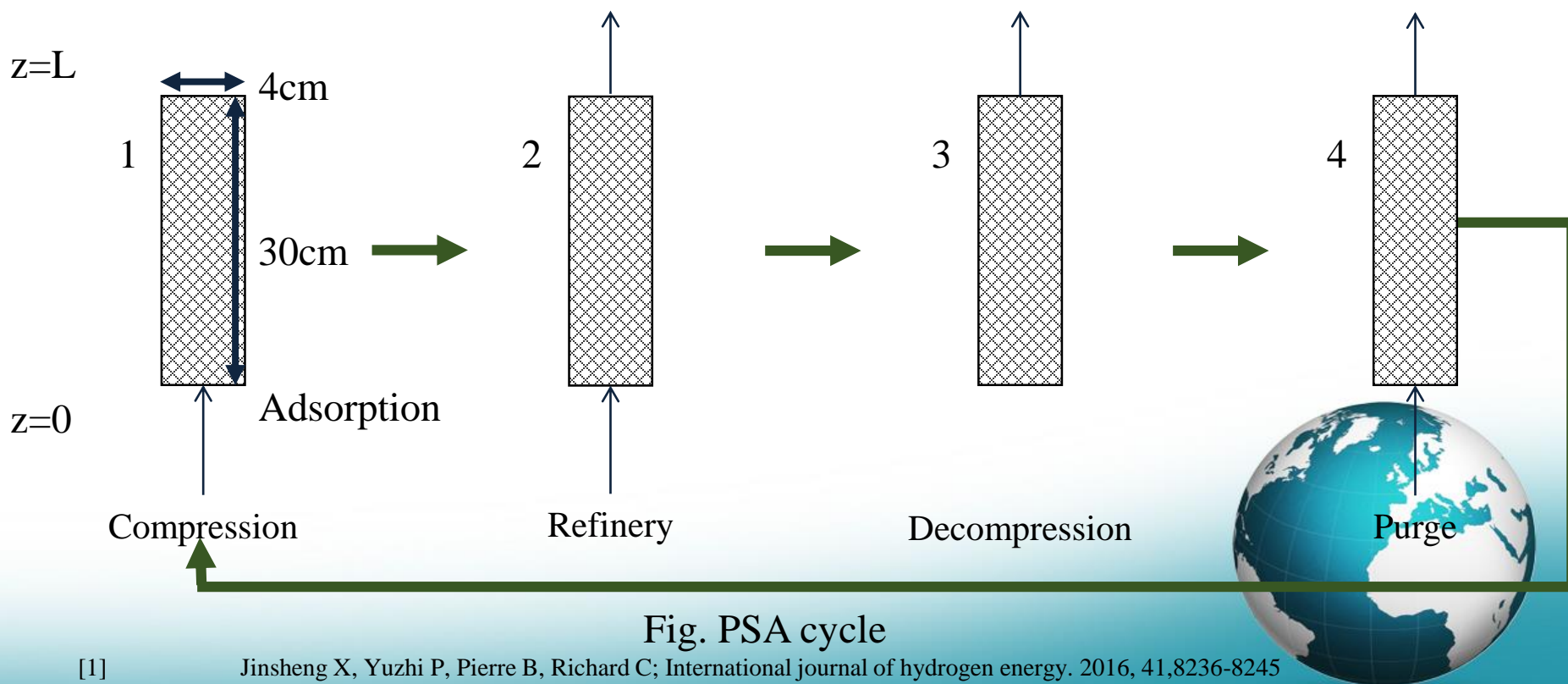


Fig. PSA cycle

- [1] Jinsheng X, Yuzhi P, Pierre B, Richard C; International journal of hydrogen energy. 2016, 41,8236-8245
 [2] Jaeyoung Yang and Chang-Ha Lee, ind. Eng . Chem. 1997, 36, 2789-2798



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✓ Results at 1st stage (HAS-Clay)

- Confirmation of selective CO₂ adsorption
- Recovery efficiencies of H₂, CO and CH₄ are higher.
- Conc. of CO₂ is high in purge process.
- CO₂ : 97.47% (adsorption efficiency)
- Temperatures in compression and refinery processes increase.
- Physical adsorption

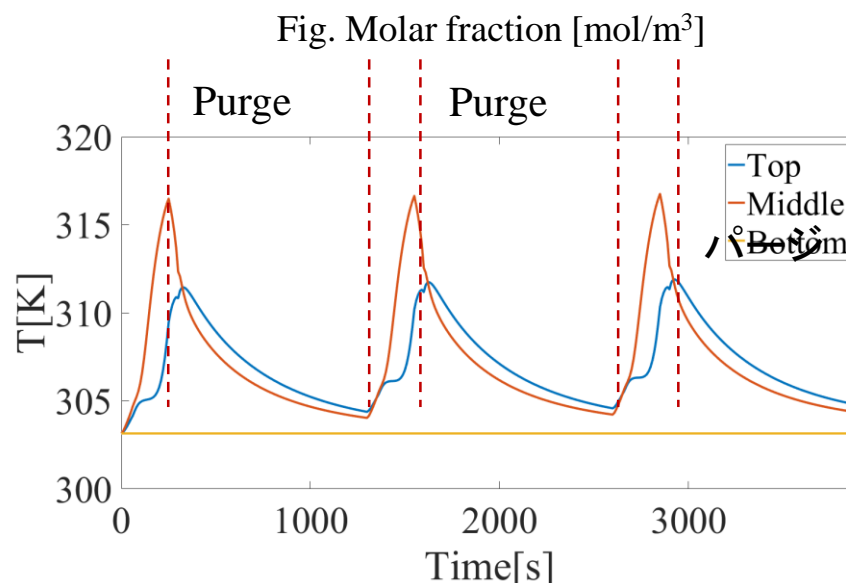
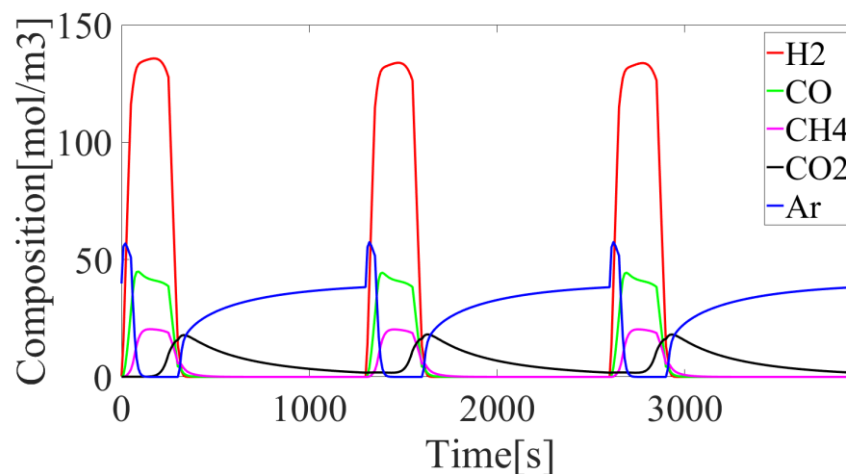


Fig. Inner temperature [K]

	H ₂	CO	CH ₄
Flow rate 1 st [%]	88.30%	88.42%	82.09%



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✓ Results at 2nd stage (Zeolite A5)

● **H₂ Conc. : 99.18%**

● **H₂ recovery eff. : 78.14%**

➤ Advantage point is to improve the product quality (concentration) in comparison to the conventional PSA without CO₂ adsorption

➤ Reduction of auxiliary power: approx. 30% abatement ^[1]

	H ₂	CO	CH ₄	CO ₂
Flow rate 2 nd [%]	99.18%	0.77%	0.04%	0.003%

Only H₂ gas can pass through.
Sequestration of H₂ can be achieved.

[1] Dowaki, K. et al.: IEEJ Transactions on Electronics, Information and Systems , **128**(2), 168-175 (2008)

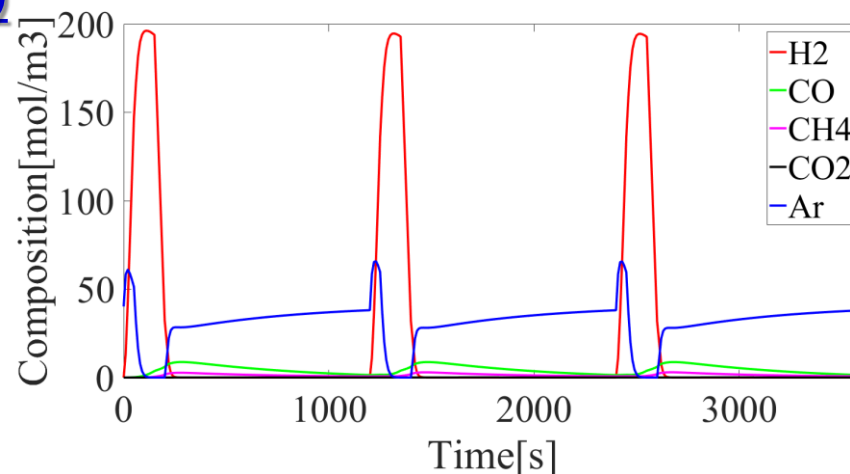


Fig. Molar fraction [mol/m³]

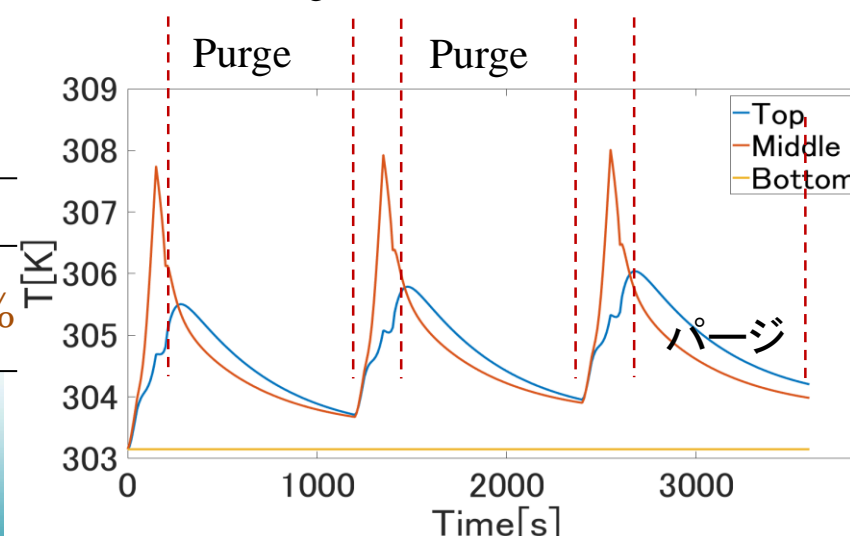


Fig. Inner temperature [K]



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✓ Impurities problems on the operation by Bio-H₂?

- Contaminations of bio-syngas: HCl, H₂S, NH₃ etc.
- FC applications→Polymer Electrolyte Fuel Cell (PEFC) (present)

1. HCl (Hydrogen chloride)

- Pt dissolution (Use of catalyst on FC electrodes)

2. H₂S (Hydrogen sulfide)

- Performance drop

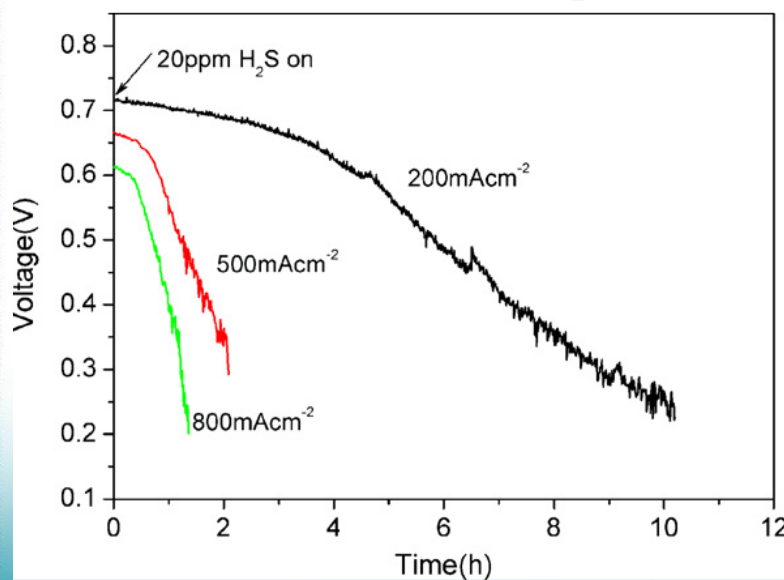


Fig. Effect of current density on the performance deterioration during exposure to 20 ppm H₂S/H₂. $T_{\text{cell}} = 70^\circ\text{C}$, humidification temperatures of the anode and cathode: room temperature and 70°C .



Source: W. Shi et al. / Journal of Power Sources 164 (2007) 272–277



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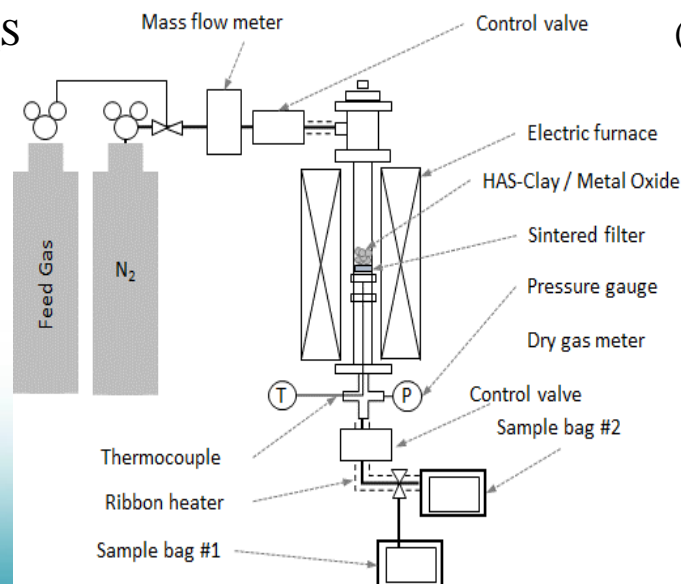
✓ Estimation of breakthrough curve (Removal Tests)

➤ Adsorbent candidates

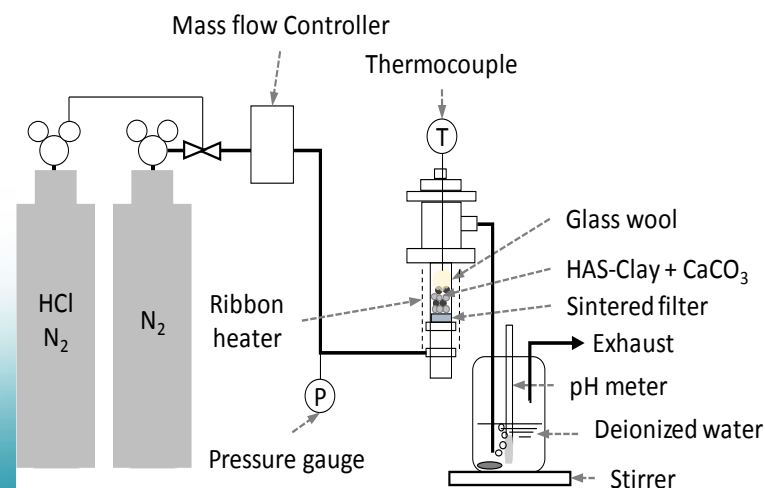
Specification	HAS-Clay	Zinc oxide	Iron oxide	Calcium carbonate
Target Impurities	H ₂ S/HCl	H ₂ S	H ₂ S	HCl
Chemical composition	SiO ₂ ·Al ₂ O ₃ ·H ₂ O	ZnO	Fe ₂ O ₃	CaCO ₃
Particle size [mm]	2.2-3.35 (H ₂ S) Powder (HCl)	2.2-3.35	2.2-3.35	12×10 ⁻³ -15×10 ⁻³
Pore diameter [nm]	<0.02	-	-	-

Note: HAS-Clay means synthetic substances of hydroxyl aluminum silicate and clay.

(a) H₂S



(b) HCl





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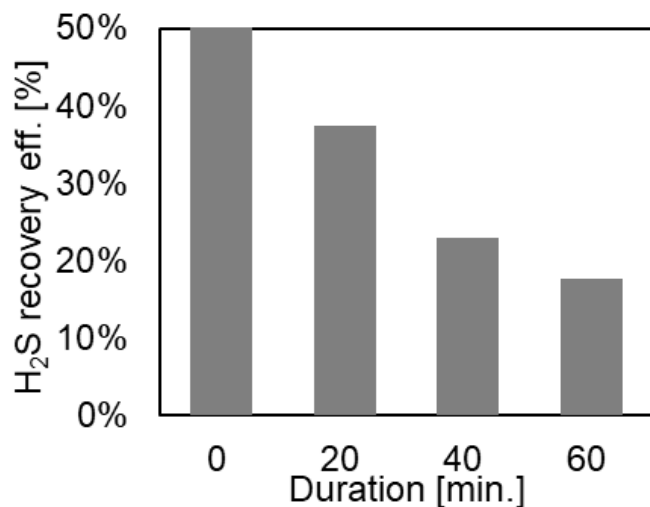
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✓ Absorption performance of HAS-Clay(Results of H_2S (1))

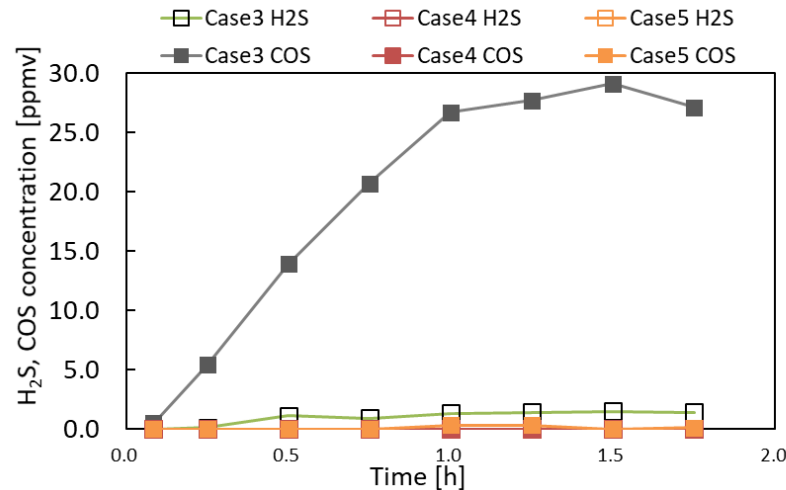
➤ Condition

1. H_2S : 30 ppmv, flow rate : 50 Nml/min. , 40 deg.C and 0.4 MPaG,
Sample weight : HAS-Clay (2 g), Space velocities (SV) : $2,915 \text{ h}^{-1}$
2. H_2S : 100 ppmv, flow rate : 250 Nml/min. , 40, 80, 120 deg.C and atmospheric pressure, Sample weight : ZnO (1.3 g) or Fe_2O_3 (0.95 g), Space velocities (SV) : $8,784 \text{ h}^{-1}$ (constant)

(a) Physical Adsorption (HAS-Clay)



(b) Physical Adsorption (Zeolite A-5)



Note:

- ✓ In 2-step PSA (the combination of HAS-Clay and Zeolite A-5), almost H_2S can be eliminated.
- ✓ Prevention of $H_2S + CO_2 = COS + H_2O$ because of an absorption of CO_2 by HAS-Clay.
- ✓ Chemical adsorption is a complementary use.

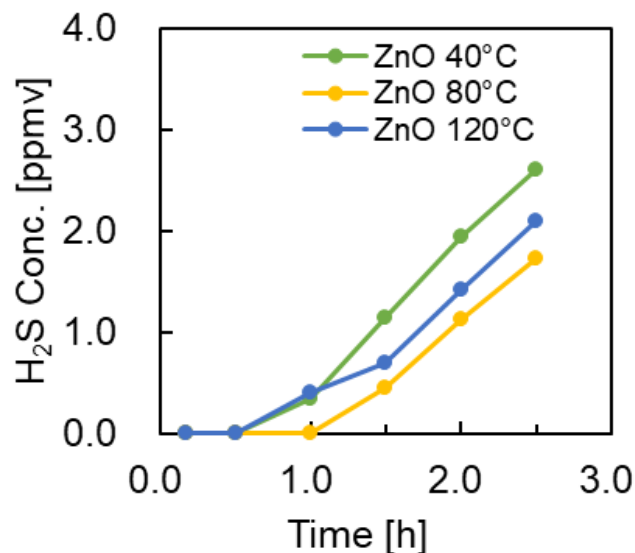


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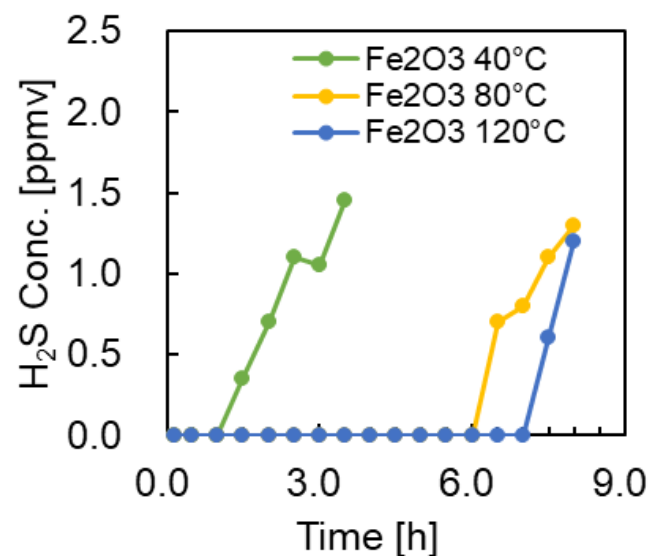
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✓ Estimation of breakthrough curve (Results of $H_2S(2)$)

(a) Chemical Adsorption (ZnO)



(b) Chemical Adsorption (Fe_2O_3)



➤ Sulfur capture capacity (Definition)

$$S_{cap} = \frac{t_{BT} \times \dot{V} \times C_{PG} \times At_{as}}{V_m \times W_{sorbent}} \times 100$$

t_{BT} : Breakthrough time [min]

C_{PG} : Conc. of pollutant [ppmv]

\dot{V} : Flow rate [L/min]

V_m : Molar volume [L/mol]

At_{as} : Atomic weight (=32.07)

$W_{sorbent}$: Adsorbent weight [g]

Table Sulfur capture capacity

Temp. [°C]	ZnO*	$Fe_2O_3^*$
40	0.24	0.54
80	0.31	1.65
120	0.28	1.69

*Unit: g-S/100 g-sorbent



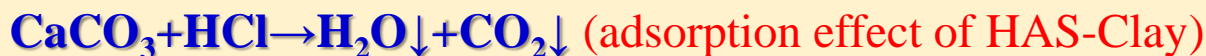
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✓ Absorption performance of HAS-Clay(Results of HCl(1))

➤ Condition

1. HCl: 1,160 ppmv, Flow rate: 200 Nml/min, 100-200 deg.C and atmospheric pressure
Sample weight : HAS-Clay (0.1 g) and/or CaCO₃(1.0g)
Space velocities (SV) : 3,725-32,000 h⁻¹ (see **Table**)
2. Estimation of the effect of blend effect vs. mono-adsorbent.



Note: In general, Ca based adsorption is worked at the temp. of >600 deg.C.

Table Combination of samples and SVs

	Specimen		
	#1	#2	#3
CaCO ₃ [g]	1.00	0.00	1.00
HAS-Clay [g]	0.00	0.10	0.10
Space Velocity [h ⁻¹]	4,216	32,000	3,725

Based on the experimental results, the estimation of adsorption effect of blend case (Cl capture) was carried out.



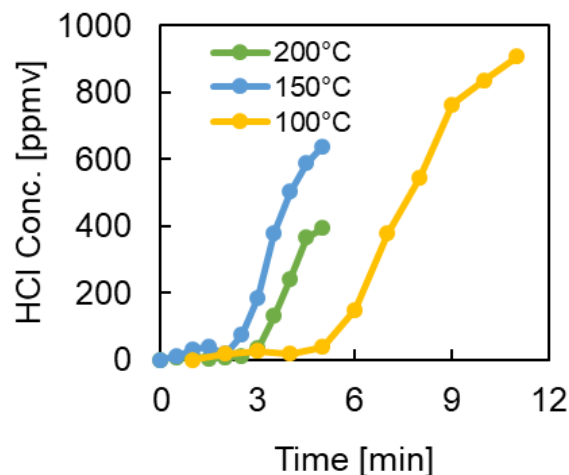


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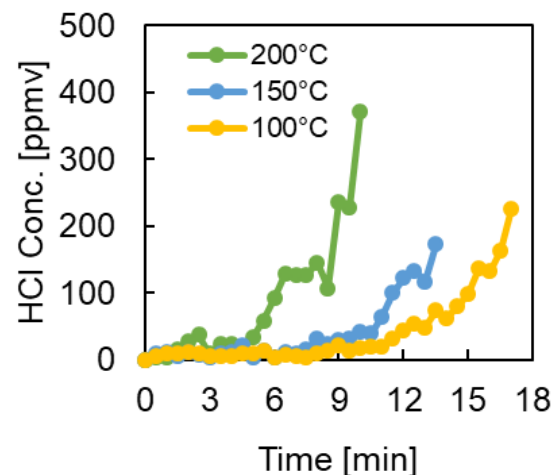
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✓ Estimation of breakthrough curve (Results of HCl (2))

(a) CaCO_3



(b) HAS-Clay



(c) Blend

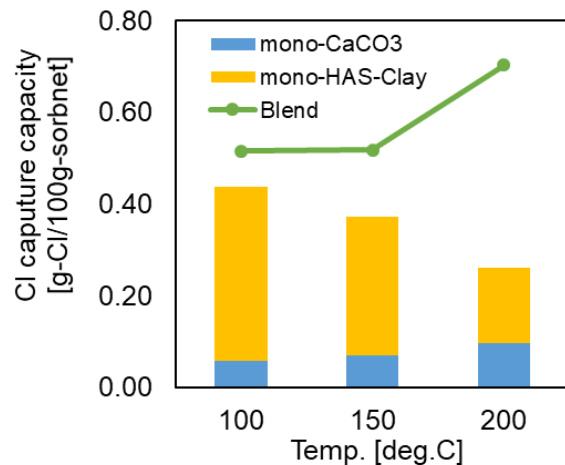


Table Chlorine capture capacity

Temp. [°C]	CaCO_3^*	HAS-Clay*	Blend*
100	0.06	4.18	0.52
150	0.08	3.32	0.52
200	0.11	1.79	0.70

*Unit: g-Cl/100 g-sorbent



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✓ Impact analysis

➤ Purpose

1. Due to reduction of amount of chemicals (adsorbent), the eco-burden in consideration of LCA is to be visualized.

➤ Conditions

1. Functional unit: 1 Nm³ Bio-H₂ (4N)
2. Estimated Index: Abiotic metal depletion potential (ADP), global warming potential (GWP)
3. Software: SimaPro 8.2 software (Impact analysis: the Centrum voor Milieukunde Leiden (CML) method)
4. Conventional case (H₂S): ZnO (Conv. ZnO) (Capture capacity: 2.81 g-S/100 g-sorbent)
5. Initial concentration (H₂S): 200 ppmv
6. Proposed case: 2-step PSA+ZnO (0.24 g-S/100 g-sorbent), PSA+Fe₂O₃ (0.54 g-S/100 g-sorbent) *Note: Temp. 40 deg.C
7. Conventional case (HCl): Na₂CO₃ (Conv. Na₂CO₃) (Capture capacity: 5.35 g-Cl/100 g-sorbent)
8. Proposed case (Blend case): HAS-Clay+CaCO₃ (0.70 g-Cl/100 g-sorbent)
9. HAS-Clay is assumed to be regenerable.
10. Calculation

$$\text{Impact Potential} = \text{Inventory Value} \times \text{Characterisation Factor}$$

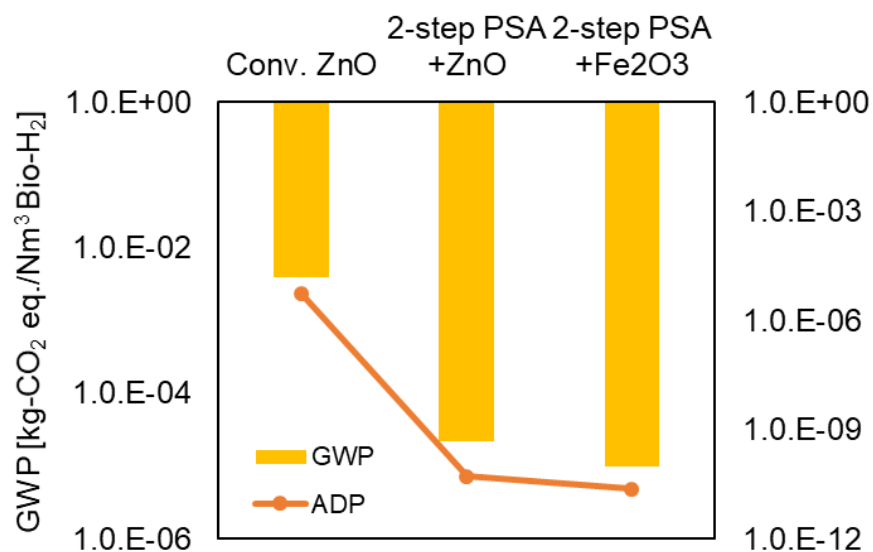


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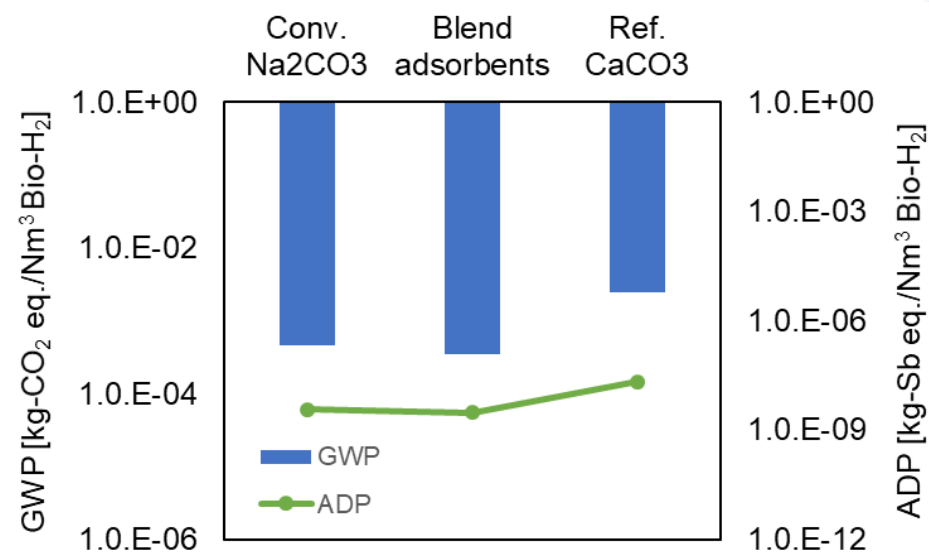
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✓ Estimation of GWP and ADP

(a) H_2S



(b) HCl



□ Advantages due to HAS-Clay use

- The eco-indexes of GWP and/or APD was remarkably improved in comparison to the conventional cases (H_2S).
- In the case of blend of HAS-Clay and $CaCO_3$, GWP and ADP in comparison to the conventional case were improved by 25.4 % and 19.4 %, respectively (HCl).



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✓ Conclusions

- In our group, Bio-H₂ production system using the gasification process of Blue Tower is developing.
- The design policy is based on LCA indexes to obtain the eco-benefit of biomass feedstock.
- Looking at the entire system, the key technology is the reduction of external energy consumption besides an assurance of steady operation.
- Also, the technology of impurities removal would be extremely important to match a fuel specification for FC application.
- In this case, the candidates have to be selected appropriately, since the adsorbents are associated with eco-burden.





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✓ Conclusions (continued)

- HAS-Clay which we concerned in this study has good potentials to reduce the auxiliary power and eliminate the impurities in product gas.
- The characteristic of HAS-Clay, especially, CO_2 adsorption, can promote the elimination of H_2S and HCl , too.
- Simultaneously, the consumption of metal oxide would be reduced due to these characteristics.
- Using the eco-index on basis of LCA (GWP and ADP), the obvious advantages can be obtained.
- In our future tasks, the adsorption performance of other impurities (e.g. NH_3) will be analyzed.





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